



UNIVERSIDADE ESTADUAL DE CAMPINAS
SISTEMA DE BIBLIOTECAS DA UNICAMP
REPOSITÓRIO DA PRODUÇÃO CIENTÍFICA E INTELLECTUAL DA UNICAMP

Versão do arquivo anexado / Version of attached file:

Versão do Editor / Published Version

Mais informações no site da editora / Further information on publisher's website:

https://www.scielo.br/scielo.php?script=sci_arttext&pid=S0103-90162018000600445

DOI: 10.1590/1678-992X-2016-0456

Direitos autorais / Publisher's copyright statement:

©2018 by Universidade de São Paulo/Escola Superior de Agricultura "Luiz de Queiroz".
All rights reserved.

DIRETORIA DE TRATAMENTO DA INFORMAÇÃO

Cidade Universitária Zeferino Vaz Barão Geraldo

CEP 13083-970 – Campinas SP

Fone: (19) 3521-6493

<http://www.repositorio.unicamp.br>

On the controlling of temperature: A proposal for a real-time controller in broiler houses

Denise Trevisoli Detsch^{1*}, Dante Conti², Maria Aparecida Diniz-Ehrhardt², José Mario Martínez²

¹Federal University of Paraná – Department of Engineering and Exact, R. Pioneiro, 2153 – 85950-000 – Palotina, PR – Brazil.

²State University of Campinas/Institute of Mathematics, Statistics and Scientific Computing – Dept. of Applied Mathematics, R. Sérgio Buarque de Holanda, 651 – 13083-859 – Campinas, SP – Brazil.

*Corresponding author <denise.detsch@ufpr.br>

Edited by: Thomas Kumke

Received November 16, 2016

Accepted October 30, 2017

ABSTRACT: Environmental conditions in broiler houses, specifically temperature, are key factors that should be controlled to ensure appropriate environment for broiler rearing. In countries with tropical/subtropical climate, like Brazil, high temperatures produce heat stress to animals, affecting the production process. This research proposes a real-time model to control temperature inside broiler houses. The controller is a self-correcting model that makes real-time decisions on the ventilation system operation (exhaust fans) together with temperature prediction at the facility. The model involves partial differential equations (PDE) whose parameters are updated according to data registered in real-time. Some experiments were carried out at a pilot farm in the municipality of Jundiaí, São Paulo State, Brazil, for different periods during winter and summer. The results based on simulations in comparison with the current automatic ventilation system show that the model is consistent to keep temperature under control for an efficient production. The model achieved a bias of 0.6 °C on average in comparison with the ideal temperature, whereas the automatic controller measured a bias of 3.3 °C, respectively. Future lines suggest that this approach could be useful in many other situations that involve environmental control for livestock production.

Keywords: partial differential equations (PDE), temperature control, optimization, self-correcting model, ventilation systems

Introduction

Poultry production provides animal protein to many people worldwide. Chickens adapt to most areas, are relatively inexpensive and have a high productivity rate. Most poultry production uses intensive farming techniques that involve sophisticated decisions (Reboiro-Jato et al., 2011). However, in regions with tropical/subtropical climate, like Brazil, broiler rearing is commonly affected by high temperature values, affecting the production by causing heat stress and high mortality rates (Renaudeau et al., 2012). In addition, chickens are housed in facilities where environmental conditions are monitored and controlled by automatic systems to achieve ideal temperature conditions to maximize production. In particular, depending on the broiler age/breed, well-established standards indicate that ideal temperatures that should be kept inside the houses (Cobb-Vantress, 2012; Yahav et al., 2004). Temperatures out of standards affect the thermal comfort of the animals, which could lead to less weight gain, feed efficiency and high mortality rates (Donkoh, 1989; Razuki et al., 2011). Nowadays, automatic systems are crucial to ensure effective stability to microclimate conditions in the facilities (Bustamante et al., 2013). However, in Brazil, many farmers still produce without sophisticated controllers and perform their activities by controlling the ventilation system with basic controllers or even manually.

Therefore, this research proposes a model to support temperature control by assisting the ventilation system with decision-making in real-time and tempera-

ture prediction at the facility. Most automatic controllers are reactive and act according to current data with pre-established rules, without tools for forecasting or self-learning. This study describes a complete framework to deal with the problem that combines applied mathematics, self-correcting and real-time response. The paper starts presenting materials and methods. Then, the pilot farm and experiments are presented with the results and discussion. Finally, additional considerations and future works are listed.

Materials and Methods

Introducing the model

Temperature in a broiler house at time $t + \Delta t$ is a function of external temperature, internal temperature at time t , controls of heating, ventilation or cooling equipment, as well as a number of unknown parameters that should be fitted in the best possible way to replicate the real behavior of the system.

Decisions about the controls at instant t_0 (initial time) should be taken according to a prediction of the system state along a reasonable period $[t_0, t_f]$, that is, from initial time t_0 to final time t_f . This "reasonable" period $t_f - t_0$ minutes (typically, 1 h) with a number of intervals n (typically, $n = 10$, that is, 6 min each) is set by assuming that this temporal granularity could fit the real-time approach of the model considering feasibility, response to support the ventilation system and the intrinsic dynamics of the thermal conditions inside the broiler houses, as suggested by experts consulted during the research.

The prediction of the external temperature in $[t_0, t_f]$ may be obtained from meteorological forecasting, whereas internal temperature during this period and for different possible controls needs a mathematical model.

Assuming that such a mathematical model is available, the controls should be chosen to optimize the temperature throughout the period $[t_0, t_f]$. This means that the model that predicts the internal temperature should be run many times to have the closest predicted temperatures in relation to the ideal ones.

The essence of the mathematical prediction model is to foresee the behavior of the environment at $t + \Delta t$ for all t in $[t_0, t_f]$ by using the system state at instant t . This problem naturally leads to models that are based on partial differential equations (PDE). Strictly speaking, the natural model should involve PDE of a complex Fluid Mechanics problem in three spatial dimensions. However, this model should be run many times to check different control strategies; therefore, standard Computational Fluid Dynamics (CFD) procedures are not affordable since they could not solve the whole problem in real time, as required by the application (Anderson, 1995; Fletcher and Fletcher, 1988; Rojano et al., 2015). Some radical simplifications of the problem are necessary to obtain a reasonable and practical prediction of the model. This research presented simplifications for a consistent control model for the improvement of environment conditions of temperature control for poultry production.

Fluid mechanics models rely on very complex representation of 3D (or, perhaps, 2D) phenomena to reproduce real behavior as well as possible. However, the necessity to predict temperature in real time

inhibits the possibility of using such models due to time response and computational costs. Therefore, our proposal focused on developing a model that could be solved under real-time conditions by allowing self-correction of parameters and reflecting the physical characteristics of the phenomenon. The decision for the model approximation degree to reality is crucial and depends on practical goals of the modeling process. Thus, our objective is not the accurate approximation of the model to the phenomenon, but its capacity to make satisfactory decisions from a practical viewpoint.

Prediction model and conceptual algorithm

Model

For a better understanding of the model, Table 1 summarizes the set of symbols, parameters and acronyms used in this proposal.

Consider a broiler house with a longitudinal wall (called here as "segment") $[0, L] \subset \mathbb{R}$ where L represents the facility length and a is the wall thickness. Two segments, $[-a, 0]$ and $[L, L + a]$ represent the left-wall and right-wall, respectively. The diffusion coefficient in the walls is called σ_w and the diffusion coefficient in the broiler house is called σ_a . In addition, the control devices increase or decrease internal temperature u degrees per time unit, where $u = u(x, t)$ is a function that depends on control decisions. This leads to the following diffusion problem:

$$\frac{\partial T}{\partial t}(x, t) = \sigma_w \frac{\partial^2 T}{\partial x^2}(x, t) \text{ if } x \in [-a, 0] \quad (1)$$

Table 1 – List of symbols, parameters and acronyms of the proposed controller.

Symbol/Parameter/Acronym	Description	Unit of measurement
t	Time	min
t_0	Initial time	min
t_f	Final time	min
Δt	Interval of time	min
L	Length of the facility	m
a	Thickness of the wall	m
σ_w	Diffusion coefficient in the walls	$m^2 \text{ min}^{-1}$
σ_a	Diffusion coefficient in the broiler house	$m^2 \text{ min}^{-1}$
u	Control function of internal temperature	$^{\circ}\text{C}$
x	Position in broiler house	m
T	Temperature	$^{\circ}\text{C}$
T_{ideal}	Ideal temperature desired for the broiler house	$^{\circ}\text{C}$
d_j	Number of control devices	
N	Number of devices	
α	Increase of internal temperature in the absence of connected exhaust fans	$^{\circ}\text{C per unit time}$
β	Decrease of internal temperature per activation of each fan	$^{\circ}\text{C per unit time}$
n	Number of intervals for simulation	
δ	Simulation time	min
PDE	Partial Differential Equations	
CFD	Computational Fluid Dynamics	

$$\frac{\partial T}{\partial t}(x, t) = \sigma_a \frac{\partial^2 T}{\partial x^2}(x, t) - u(x, t) \text{ if } x \in [0, L] \quad (2)$$

$$\frac{\partial T}{\partial t}(x, t) = \sigma_w \frac{\partial^2 T}{\partial x^2}(x, t) \text{ if } x \in [L, L + a] \quad (3)$$

$$T(x, 0) \text{ given for all } x \in [-a, L + a] \quad (4)$$

$$T(-a, t) = T(L + a, t) \text{ given for all } t \geq 0 \quad (5)$$

$$\frac{\partial^2 T}{\partial x^2}(0, t) = \frac{\partial^2 T}{\partial x^2}(L, t) = 0 \text{ for all } t \geq 0 \quad (6)$$

In other words, Equations (1) to (6) represent a diffusion problem (Welty et al., 2008) in the segment $[-a, L + a]$, where the diffusion coefficients are σ_w and σ_a in different regions. A boundary condition represents the external temperature and an initial condition that represents the initial temperature of the broiler house. Moreover, the temperature $T(x, t)$ at the facility decreases if control $u(x, t)$ is greater than zero, and increases otherwise.

The control function depends on the control devices. These control devices have a finite number of possible states d_0, d_1, \dots, d_N . For example, d_j may indicate that the number of connected exhaust fans is j , by assuming that exhaust fans are the only control devices in the broiler house under analysis. A function $u_{d_j}(x, t)$ is associated to each possible control state d_j :

$$u_{d_j}(x, t) = \alpha - j\beta \quad (7)$$

Therefore, in the absence of connected exhaust fans, internal temperature tends to increase α degrees per time unit, but the activation of each fan decreases the temperature β degrees per time unit.

The following conceptual algorithm describes how decisions are made. The algorithm runs on a continuous basis during the life of the broiler house (whole process of broiler rearing).

This algorithm is "conceptual" because, for the sake of simplicity, details concerning discretization and location of sensors are omitted. Inputs associated to the algorithm are: T_{ideal} , temperature that depends on the age of chickens and type of the broiler house. The well-established value seeks to achieve thermal comfort of the animals to maximize their biological response and, therefore, weight gain. Moreover, it is assumed that L, a, σ_w, σ_a and the functions u_j are given for all $j = 0, 1, \dots, N$. To fix date, time is measured in minutes and execution of the algorithm starts when real "clock time" is t_0 . A simulation time is established of $t_f - t_0$ minutes (typically, one hour) and a number of intervals for simulation n (typically, $n = 10$). Thus, δ is defined as follows:

$$\delta = (t_f - t_0) / n \quad (8)$$

Conceptual algorithm

Step 1 – Establish initial and boundary conditions: Using

appropriately located sensors, interpolations and weather forecasting, establish the initial conditions for temperature at the facility and walls, as well as the boundary conditions that concern the external temperature from time t_0 to t_f ,

Step 2 – Trial controls: Choose "trial controls" d_{i1}, \dots, d_{in} , where $d_{ik} \in \{d_1, \dots, d_N\}$ for all $k = 1, \dots, n$.

Step 3 – Solve the PDE: Solve the problem (Equations 1 to 6) from $t = t_0$ to $t = t_f$, considering that the source function $u(x, t)$ is determined by the choice of d_{i1}, \dots, d_{in} in Step 2. Namely, in the solution process of Equations 1-6, assume that for all $k = 1, \dots, n$, if $t \in [t_0 + (k-1)\delta, t_0 + k\delta]$ the function $u(x, t)$ is the one that corresponds to the control state d_{ik} .

Step 4 – Determine the score of the sequence of controls $\{d_{i1}, \dots, d_{in}\}$: Considering the values of the predicted temperatures $T(x, t_0 + k\delta)$ for $x \in [0, L]$ and $k = 1, \dots, n$, computed in Step 3, compute a score for the sequence of controls decided in Step 2. If this score is not satisfactory yet, go to Step 2 to simulate the behavior of the system under new controls, or else, proceed to Step 5.

Step 5 – Implement the control, save for learning and stop, proceed implementing the control d_{i1} and save $T(x; t_0 + \delta)$, $x \in [0, L]$. After δ units of real time, also save the real temperature inside the broiler house. Stop.

A flowchart of the conceptual algorithm is shown in Figure 1.

Note that the algorithm decides the best sequence of controls along the interval of real time $[t_0, t_f]$, but it only imposes the implementation of the control computed for the first interval $[t_0, t_0 + \delta]$. On one hand, considering the whole interval $[t_0, t_f]$ to make decision instead of using merely $[t_0, t_0 + \delta]$ prevents of making greedy decisions based only on the initial state at the facility, which could lead to overcooling or overheating. On the other hand, only the control decided for $[t_0, t_0 + \delta]$ deserves to be implemented in practice, as new data are coming permanently to the system that allows repeating the simulations with better knowledge of the real environment.

After stopping the algorithm, the control d_{i1} is implemented and "we wait" δ units of real time before updating t_0 and t_f for running the algorithm again. This means that δ is the number of time units in which the broiler house is subject to the control d_{i1} before a new control optimization.

Optimization and learning

Optimization appears twice in the context of the algorithm implementation. The optimal choice of the controls d_{i1}, \dots, d_{in} that maximizes the score comes from an optimization procedure whose characteristics depend on the type of control devices available in the broiler

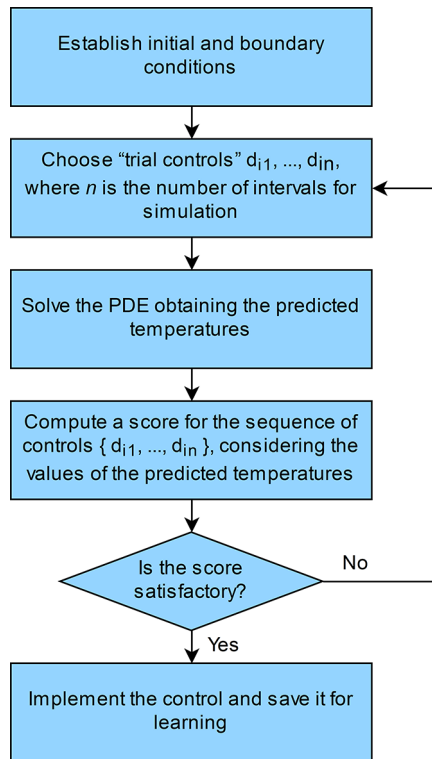


Figure 1 – Flowchart of the conceptual Algorithm.

house. For example, if all the devices are exhaust fans and their number is N , the controls d_{ik} can take the discrete values $\{0, 1, \dots, N\}$, corresponding to the number of exhaust fans connected at each δ -interval. Therefore, the optimal controls are chosen from a set that contains $(N + 1)^n$ elements. For this case, it was adopted sequential coordinate search (Conn et al., 2009) as standard algorithm to obtain local optima. The score to be maximized takes into account the predicted temperatures at times $t_0 + \delta, \dots, t_0 + n\delta$. If T_{ideal} is the ideal temperature desired for the broiler house, the score takes into account the approximation of inner temperatures to T_{ideal} along the instants $t_0 + k\delta$. These approximations are weighted in a decreasing way with respect to k by maximizing the score given by:

$$-\sum_{k=1}^n (n+1-k) |\bar{T}_k - T_{ideal}| \quad (9)$$

where \bar{T}_k is an average of the predicted temperatures in the sensors located in $[0, L]$ at time $t_0 + k\delta$.

The second instance where optimization appears is the Learning Process where the PDE model improves its ability to predict the real behavior of the system. In Step 5 of the algorithm, the predicted temperature at $t_0 + \delta$ was saved and since the algorithm normally runs in much less than δ time units, the real temperature at $t_0 + \delta$ is saved later. Therefore, the real temperature can be compared against the predicted temperature every δ time unit. Obviously, it is desired that these two vectors

of temperatures should be as close as possible. Thus, it is possible to modify the diffusion coefficients σ_w and σ_a and the dependence of u with respect to d in such a way that the difference between predicted and real temperatures is reduced. For this reduction, an additional optimization procedure is applied. As far as the algorithm runs in a real broiler house, these data allow successive improvements of the model, which, in turn, should improve efficiency of the control decisions. In other words, the model learns how to become more and more accurate during the execution of the algorithm.

Computational implementation

Solving the PDE

To solve the PDE (Equations 1 to 6), a straightforward implicit difference scheme is implemented (Le Veque, 2007), which allows to use rather large values of time discretization preserving stability (Le Veque, 2007). The initial condition is obtained from measurements in several sensors (typically three) distributed in the broiler house followed by interpolation to get the initial temperature in $[0, L]$. The initial temperature within the walls is computed interpolating external and internal temperatures at the extremes of $[0, L]$. The boundary condition is given by the external temperature obtained from forecasting at the weather station. The PDE must be solved for all trial controls d_{i1}, \dots, d_{in} . After the solution of each PDE for different controls is achieved, a score given by Equation (9) is attributed to trial d_{i1}, \dots, d_{in} . Successive trials, commanded by the coordinate-search scheme, lead to the computation of the effectively activated control d_{ii} . Finally, the left-wall is represented by the segment $[-a, 0]$, where the right-wall is the segment $[L, L+a]$. Therefore, a is the thickness of both walls. In this model, diffusion in both walls has identical coefficients, which are system parameters. In practice, the real value of a is not relevant and may be fixed arbitrarily, guided by numerical safeguards, since the effect of the walls is combined with the fitted diffusion parameters. Roughly speaking, under the accuracy degree of this model, a thick wall with a big diffusion coefficient has similar effect as a thin wall with a small diffusion coefficient. In other words, different combinations of thickness and diffusion produce analogous temperature effects within the broiler house thus the precise determination of the diffusion within walls is not relevant.

Learning algorithm

Since the control d_{ii} , the optimization product of controls in Step 4 is effectively activated, after δ units of time, current measurements of temperature in the broiler house are made, allowing to compare the measured and predicted temperature by the PDE model. The measured temperature should be as close as possible to the predicted one. Unfortunately, this is not the case, especially in the first stages of the effective system implementation in a broiler house. The Learn-

ing Algorithm modifies the model parameters σ_w , σ_a and the dependence of u with respect to d_i , for the predicted temperature at $t_0 + \delta$ coincides as much as possible with the real one obtained by the sensors. Moreover, it is not admissible abrupt modifications of the previous used parameters, which, especially after some hours of execution in the real environment, have already been the object of adjustments. For this reason, this Learning Algorithm consists of trying local random variations (10 % at most) around the already used parameters.

Calibration

Calibration is an optional procedure that can be executed at any time during the algorithm operation, assuming that data on external and internal temperatures are registered during a comparative large period (24 h) together with the controls that were implemented along that period. In the calibration procedure, one tries to find the algorithmic parameters that produce the best fit of the temperatures computed by the Algorithm to the real temperatures collected so far.

Computer requirements

The installation of the system requires a laptop computer (3.5 GHz Intel Core i7 processor and 16GB 1600 MHz DDR3 RAM memory, running OS X Yosemite-version 10.10.4) to perform calculations. Sensors are required to provide the temperature measurements in the broiler house. The model was programmed in Fortran 90. Codes were compiled by the GFortran, FORTRAN compiler of GCC (version 4.9.2) with O3 optimization directive enabled. Parameters α and β were initialized taking $\alpha = 0.02$ and $\beta = 0.01$ and are updated throughout the learning process to fit better models to new data. The other main algorithmic parameters are σ_a , the diffusion coefficient in the broiler house and σ_w , the diffusion coefficient in the wall. In this case, they were initialized to $\sigma_a = 1$ and $\sigma_w = 0.5$, but they are continuously updated according to the learning process.

The pilot farm

Experiments were carried out in one pilot poultry farm, in the municipality of Jundiaí, São Paulo State, Brazil (Latitude 23°11'11" S, Longitude 46°53'03" W). The broiler house is approximately 750 m above sea level and according to the international system of Köppen, the predominant climate in this region is Cwa (hot climate with a dry winter), with a mean air temperature of 22 °C in the hot season, and 15 °C in the cold season (registered by a local weather station managed by the Brazilian Institute of Meteorology).

The facility is the type Blue House (BH): the ventilation system with negative pressure with an automatic controller FANCONTROL CC3, cooling pad system, and roof made of fiber cement, automatic feeding and drinking lines. Its dimensions are: length, 150.0 m; width, 15.0 m; sidewall height 2.5 m; and flock density average of 12 birds m⁻².

Experiments

Controller simulations were performed on the pilot farm by comparing the evolution of the temperature measured by the model and the temperature registered by the automatic system when a rearing process was present. These experiments refer to different periods for different seasons of the year. Three experiments were designed and implemented.

Experiments were carried out by choosing different values of δ and $t_f - t_0$. This means that the algorithm chooses the present control, which operates the following δ minutes aiming to maximize the score in the following 10 δ min.

Results and Discussion

Experiment 1

Two typical winter days: maximum external temperature was 32 °C around 14h00 and minimum 13 °C around 06h00. The initial average temperature at the facility was 22.2 °C. The ideal temperature according to the age of the birds (31-32 d old) is 22 °C (Cobb-Vantress, 2012). Results of simulation of the controller versus temperature registered by the sensors of the automatic controller are reported in Figure 2.

During the night, when the external temperature is lower than 22 °C, both algorithms keep similar internal temperatures. In this situation, exhaust fans are typically off, then, the algorithm is virtually inactive. However, during daytime, when temperatures rise, the proposed controller shows a better performance by keeping the internal temperature always below 22.4 °C, while the automatic controller reaches 24.5 °C. Considering these temperature peaks and comparing with the ideal temperature, the maximum discrepancy (bias) of the proposed model was 0.4 °C and for the automatic controller was 2.5 °C, respectively.

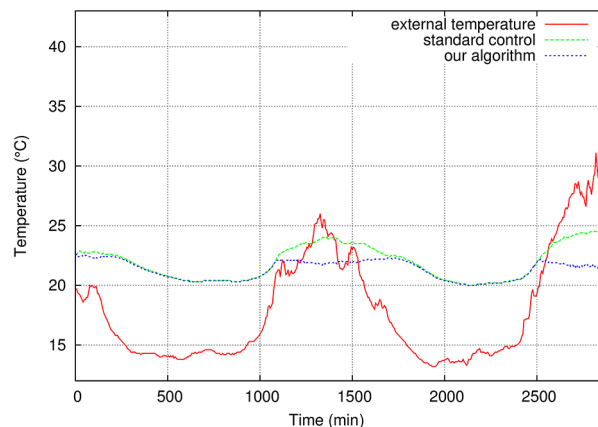


Figure 2 – Evolution of the temperatures for experiment 1 – Two typical winter days.

Experiment 2

Two typical summer days: the maximal external temperature was 37.8 °C at 13h30 and the minimal was 24.0 °C between 00h00 and 06h00. The initial average temperature in the broiler house measured at 15h00 was 22.0 °C. T_{ideal} was established at 22 °C as in experiment 1. Results are represented in Figure 3.

In this experiment, the difference between the two algorithms is clearer and more consistent. Even during the night, due to higher temperature than in the previous experiment, our algorithm shows a much better performance by keeping the internal temperature of the broiler house around 22 °C. During the day, our algorithm always keeps the internal temperature below 22.4 °C, but the standard algorithm (automatic controller) allowed the internal temperature to reach 26.0 °C. Here, the maximum discrepancy of the proposed model was again 0.4 °C and 4 °C for the automatic controller.

The main reason for these different behaviors is that our model predicts the internal temperature in a reasonably accurate way and made decisions according to predictions, whereas the standard control takes decisions only according to current measurements. In addition, these measurements could be affected for sensor problems, such as a bad calibration, noise or signal transmissions inside the automatic controller.

Experiment 3

Long-term experiment - a simulation for 24 d during winter season (final stage of the rearing process from 22 to 46 d old): the maximal external temperature was 35.6 °C and the minimal was 12.2 °C. The initial average temperature inside the facility was 22.5 °C at 15h00. Here, the average of the T_{ideal} was set at 21 °C. Results are presented in Figure 4.

Once again, the results show the advantages of this proposal compared to the standard control mechanism. Consistently, our algorithm keeps the temperature closer to ideal during daytime, while the standard con-

trol mechanism, especially on hotter days, allows internal temperature to reach 25.0 °C or even more. The discrepancy in comparison with the average of T_{ideal} was approximately 1 °C for the model and 3.5 °C for the automatic controller, respectively.

If an average is calculated from the three experiments, the proposed model obtained a discrepancy in comparison with T_{ideal} of approximately 0.6 °C and the automatic controller registered a mean value of 3.3 °C, respectively.

Finally, in this research, a real-time controller to keep and control adequate temperatures values in broiler houses was proposed. The system uses the PDE model to predict temperature inside the broiler house. The model is "semi-physical" on the sense that preserves some physical characteristics of the system, but it uses strong simplifications. Simplifications are used to allow computational implementation to be executed in real time. The optimization procedures involved in the model are fast enough to be compatible with the system operation and that the control system reacts in an adequate way to typical variations of temperature, keeping the internal temperature at acceptable levels. Its feasibility to support ventilation systems seems reasonable. Some empirical experiments have been designed to compare the model versus other automatic controllers on different farms. The proposed controller aims to provide maximum simplification of the physical phenomenon compatible with good decisions. Other controllers that could be based on linear or even nonlinear regression models may be excessively far from physical reality, whereas controllers based on full fluid mechanics are impractical for real-time predictions, considering the cost of computer devices and response time. This proposal is fully portable and may be coupled to complex engineering of different sensor architectures. Moreover, the system is adaptable to different dimensions of broiler houses due to its learning process for fitting parameters.

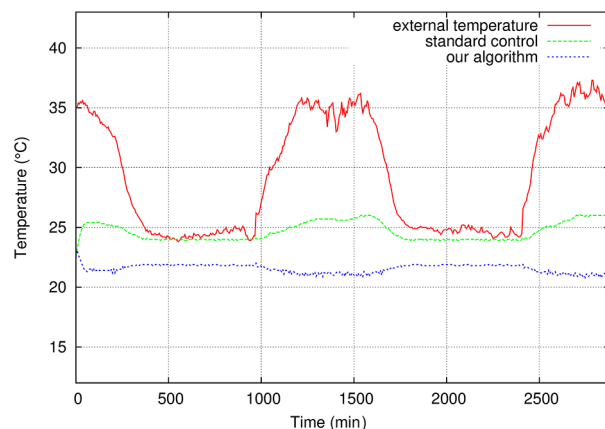


Figure 3 – Evolution of the temperatures for experiment 2 – Two typical summer days.

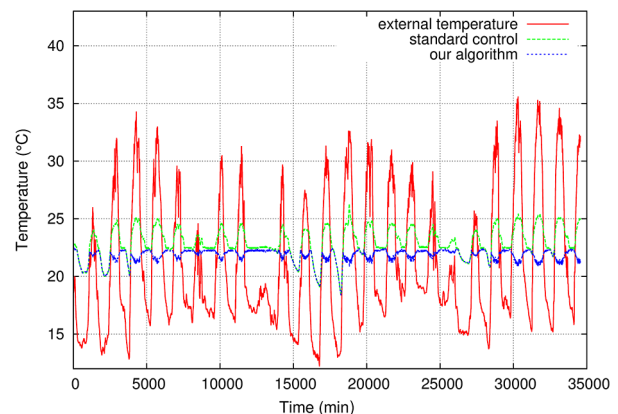


Figure 4 – Evolution of the temperatures for experiment 3 – A simulation for 24 d during winter season.

Therefore, future lines are focused on a complete evaluation of the system. These lines refer to more testing activities in the field. Although the sensitivity and stability analysis of the proposed controller is beyond the scope of this work, a theoretical analysis will be addressed in a mathematical-oriented future work, due to the importance of the topic. From the practical viewpoint, in the range of parameters that corresponds to broiler houses, stability and sensitivity seemed to be quite satisfactory.

The methodological approach used in this work can be applied in many real problems, involving complex physical phenomena, mainly in problems related to environmental control for livestock production that requires judicious simplifications for reliable modeling. Many human decisions require real-time optimization procedures and self-correcting strategies increase accuracy and help as supporting tools in the decision-making process.

Acknowledgments

This work was supported by the program Pronex of the Brazilian National Council for Scientific and Technological Development (CNPq) and Rio de Janeiro Research Foundation (FAPERJ) E-26/111.449/2010-APQ1, São Paulo Research Foundation (FAPESP) (grants 2010/10133-0, Cepid-Cemeai 2011-51305-02, 2013/03447-6, 2013/05475-7, 2013/07375-0 and 2013/21112-1) and Brazilian National Council for Scientific and Technological Development (CNPq) grant 144669/2013-7.

References

- Anderson, J.D. 1995. *Computational Fluid Dynamics: The Basics with Applications*. McGraw-Hill, New York, NY, USA.
- Bustamante, E.; García-Diego, F.J.; Calvet, S.; Estellés, F.; Beltrán, P.; Hospitaler, A.; Torres, A.G. 2013. Exploring ventilation efficiency in poultry buildings: the validation of computational fluid dynamics (CFD) in a cross-mechanically ventilated broiler farm. *Energies* 6: 2605-2623.
- Cobb-Vantress. 2012. *Broiler management guide*. Available at: <http://www.cobb-vantress.com/docs/default-source/management-guides/broiler-management-guide.pdf> [Accessed: May 31, 2017]
- Conn, A.R.; Scheinberg, K.; Vicente, L.N. 2009. *Introduction to Derivative-Free Optimization*. SIAM, Philadelphia, PA, USA. (MPS-SIAM Series on Optimization).
- Donkoh, A. 1989. Ambient temperature: a factor affecting performance and physiological response of broiler chickens. *International Journal of Biometeorology* 33: 259-265.
- Fletcher, C.A.J.; Fletcher, C. 1988. *Computational Techniques for Fluid Dynamics*. Springer-Verlag, Heidelberg, Germany.
- Le Veque, R.J. 2007. *Finite Difference methods for Ordinary and Partial Differential Equations: Steady State and Time Dependent Problems*. SIAM, Philadelphia, PA, USA.
- Razuki, W.M.; Mukhlis, S.A.; Jasim, F.H.; Hamad, R.F. 2011. Productive performance of four commercial broilers genotypes reared under high ambient temperatures. *International Journal of Poultry Science* 10: 87-92.
- Reboiro-Jato, M.; Glez-Dopazo, J.; Glez, D.; Laza, R.; Galvez, J. F.; Pavon, R.; Glez-Peña, D.; Fernandez-Rivarola, F. 2011. Using inductive learning to assess compound feed production in cooperative poultry farms. *Expert Systems with Applications* 38: 14169-14177.
- Renaudeau, D.; Collin, A.; Yahav, S.; Basilio, V.; Gourdine, J.L.; Collier, R.J. 2012. Adaptation to hot climate and strategies to alleviate heat stress in livestock production. *Animal* 6: 707-728.
- Rojano, F.; Bournet, P.E.; Hassouna, M.; Robin, P.; Kacira, M.; Choi, C.Y. 2015. Modelling heat and mass transfer of a broiler house using computational fluid dynamics. *Biosystems Engineering* 136: 25-38.
- Welty, J.; Wicks, C.E.; Rorrer, G.L.; Wilson, R.E. 2008. *Fundamentals of Momentum, Heat and Mass Transfer*. John Wiley, New York, NY, USA.
- Yahav, S.; Straschnow, A.; Luger, D.; Shinder, D.; Tanny, J.; Cohen, S. 2004. Ventilation, sensible heat loss, broiler energy, and water balance under harsh environmental conditions. *Poultry Science* 83: 253-258.